

Rectangular HTS conductors for fusion magnets

Background, motivation and design status

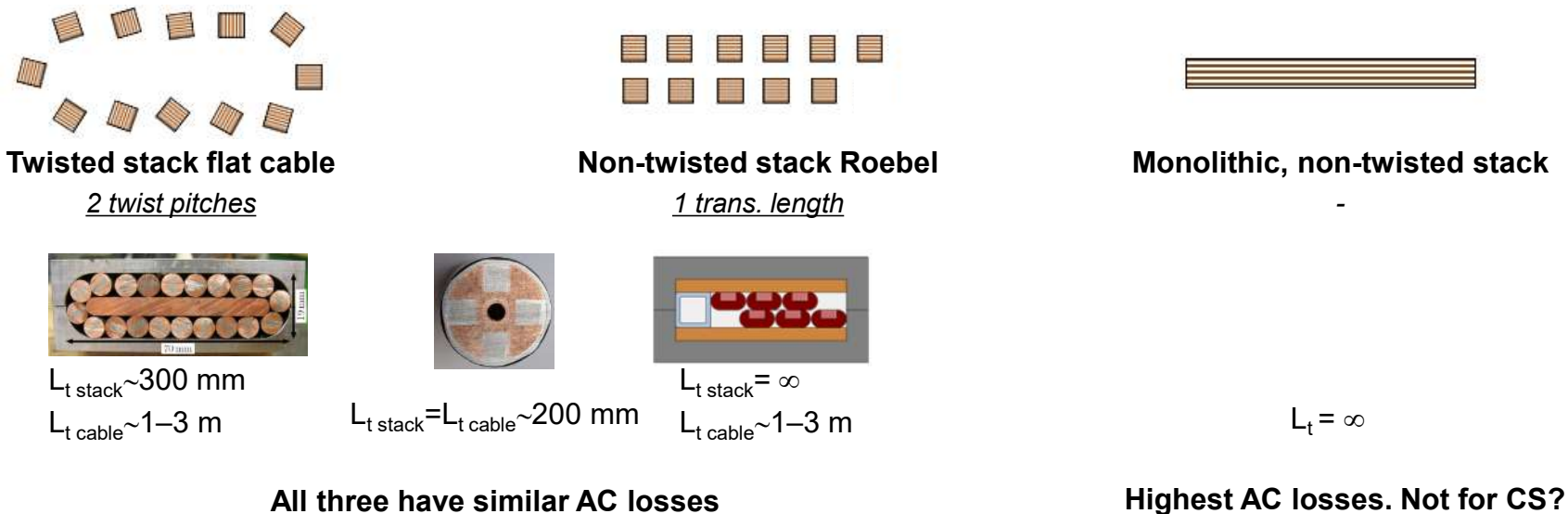
Background and motivation

HTS conductor R&D (2013-19) was focused on cables made with twisted-stack strands, because it was assumed that twisting is needed to reduce losses and current imbalance. These assumptions were never justified by a rigorous physical analysis.

In 2019 it has been shown that **twisting a stack has modest impact on losses and inductance mismatch among tapes**. <https://doi.org/10.1016/j.cryogenics.2020.103118>

The conductor space design is now much wider:

fig. 8 <https://doi.org/10.1016/j.cryogenics.2020.103118>



Abandoned by SPC because too weak and negligible advantage on AC loss

See Nikolay presentation

Next two slides

Monolithic, non-twisted stack



NIFS, 2008

<https://doi.org/10.1109/TASC.2008.922522>
<https://doi.org/10.1016/j.cryogenics.2016.06.011>

- Operation at 12 T, 20 K. Only HTS.
- <10 m long (segmented coils): current redistributes at joints (ind. imbalance); coupling currents closes at joints
- DC magnet (seldom, slowly charged): large losses ($\sim 5 \text{ MJ/m}^3$) are tolerable



EUROfusion DEMO

- Operation at 18 T, 5 K. HTS+LTS
- Km long: about inductance imbalance and losses see <https://doi.org/10.1016/j.cryogenics.2020.103118>
- AC magnet (continuously, fast ramped): does satisfy losses requirement?

A conductor for DC magnets (<0.005 T/s) may not work in AC magnets (up to 1 T/s). Could ITER TF conductor be used in the CS?

Over 10 non-twisted, non transposed concepts since 1968. Two recent examples:



T. Painter, NHFML

O1B.2-1 Thomas Painter, First test results of the integrated coil form technology, TOFE 2020



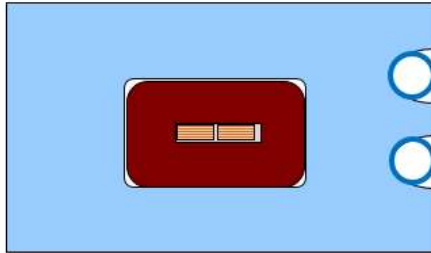


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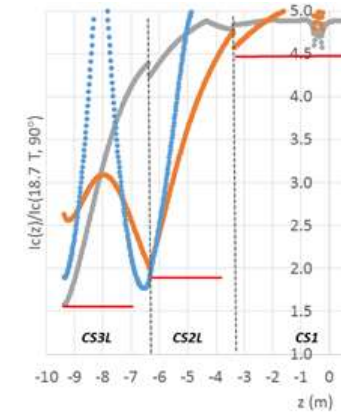
Model coil in construction now, not in 2024...

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Status of the design of monolithic, non-twisted stack for hybrid CS at SPC



*Proposed in early 2019
for the quench experiment*



What has been done?

- Selected the stack cross section (number of tapes) in all CS modules: parallelism between tapes and CS axis has a modest effect on I_c in 4 out of 5 modules. Cost reduction is negligible.
- Designed the copper elements (quench protection) to simplify manufacturing.
- Designed steel jacket for the CS conductor (grading and simplification) and SULTAN test conductor
- Studied influence of stack aspect ratio on losses and strain. Peak strain after winding on 1.5 m radius: $<0.1\%$; thermo-hydraulic analysis is needed for the aspect ratio selection.
- Measured transverse critical stress (\perp tapes): >80 MPa (about 15–50 MPa in round twisted stacks)

What is missing?

- Measure transverse critical pressure in the direction parallel to the tapes ([very high operating value](#))
- Select test configurations for full load operations in SULTAN (not necessary full size conductor).
- Submit paper about design to a journal.

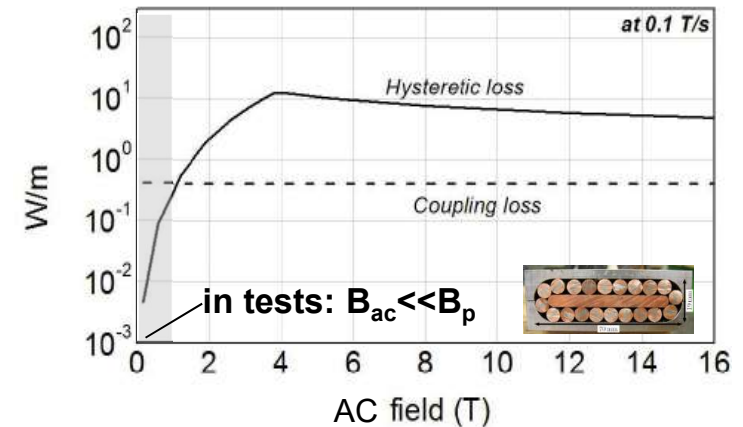
CS magnet: AC loss

AC loss is not important. It is the only thing (with fatigue of course) that matter.

Commonwealth Fusion is developing a low-loss VIPER cable for the SPARC CS.

Cables made with tapes have much larger losses than multifilamentary cables (<1 T/s). The main contribution is hysteretic loss (eff. fil. $\varnothing \sim 1000 \mu\text{m}$ instead of $10\text{--}30 \mu\text{m}$).

Could the CS be wound with $200 \mu\text{m}$ filaments Nb_3Sn strands?



Small scale version of the hybrid CS (similar field, J_c , geometry): 25 T cryogen-free solenoid at Tohoku University. **Losses (W/m^3) in HTS insert are $10\text{--}100\times$ higher than in the LTS outsert.** <https://doi.org/10.1109/TASC.2014.2366552> <https://doi.org/10.1016/j.cryogenics.2016.05.010>

No need to wait for tests. Thermo-hydraulic analysis could start any time.

- Peak temperature in the winding: 6 K, 15 K, 30 K, ...? (I_c reduces by 50% from 5 K to 20 K)
- Can the monolithic, non-twisted stack be used in CS?
- Optimal stack aspect ratio?